Energy-Tailorable Spin-Selective Multifunctional Metasurfaces with Full Fourier Components

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Compact integrated multifunctional metasurface that can deal with concurrent tasks represent one of the most profound research fields in modern optics. Such integration is expected to have a striking impact on minimized optical systems in applications such as optical communication and computation. However, arbitrary multifunctional spin-selective design with precise energy configuration in each channel is still a challenge, and suffers from intrinsic noise and complex designs. Here, a design principle is proposed to realize energy tailorable multifunctional metasurfaces, in which the functionalities can be arbitrarily designed if the channels have no or weak interference in k-space. A design strategy is demonstrated here with high-efficiency dielectric nanopillars that can modulate full Fourier components of the optical field. The spin-selective behavior of the dielectric metasurfaces is also investigated, which originates from the group effect introduced by numerous nanopillar arrays. This approach provides straightforward rules to control the functionality channels in the integrated metasurfaces, and paves the way for efficient concurrent optical communication.

As there has been rapid development of modern fabrication techniques, integrated planar electromagnetic (EM) functional systems have been considered as one of the most challenging research fields in theory and technology. In the past decades, planar integrated manipulation of EM waves has been investigated at different wavebands, such as microwave,[11] terahertz,[2,3] and infrared[4] regions. Artificial metasurfaces composed of customized planar nanostructures have been a research hot spot to manipulate EM waves, which provide a wide platform for deep light–matter interactions at the subwavelength scale.[5–10] Taking advantage of the abundant resonances generated from nanostructures composed of different materials, such as metallic,[11] dielectric,[12,13] and 2D materials,[14] various kinds of metasurfaces have been proposed in the applications of electromagnetically induced transparency,[15] zero-index responses,[16,17] asymmetric spin-orbit interaction,[18,19] structural colors,[20–23] surface waves,[24] topological photonics,[25,26] and so on. Metasurfaces are also a sophisticated and versatile tool to control optical amplitude,[27] phase,[28] polarization,[29] and the combination of these optical dimensions.[30–33] Compared with single-layer metasurfaces, few-layer metasurfaces with two or more overlapping structure layers significantly increase the effective light–matter interaction distances and exploit the integrated functionalities of metasurfaces.[34–39] However, to date the integration of arbitrary optical functionalities onto one single metasurface is still challenging due to the limitation of theoretical design and the absence of full control for multidimensional optical fields.

Recently, integrated multifunctional metasurfaces that can deal with concurrent tasks have drawn much attention of the scientific community.[40–43] One of the designs to realize multifunctional metasurfaces is to divide the device into several areas, and each area serves as one functionality.[44,45] Such designs usually suffer from low information capacity and strong noises originated from channels mixing.[46] Another design utilizes harmonic analysis to distribute all the functionality channels to each nanostructures, which has been widely investigated to achieve polarization-controllable multichannel vortex beams generation.[47–49] Jiang et al. proposed a broadband multipole vortex beams generation for centimeter waves, and opened up the possibilities for multichannel information gigahertz modulation.[50] However, the abovementioned designs employ intensity- or phase-only manipulation to control the optical fields, which suffer from unavoidable noises for multifunctional optical devices. Especially for the phase-only design,[51] one usually needs to perform complex optimizations...
and iteration operations to maximize the efficiency, which is time-consuming and the efficiency is theoretically limited due to the existence of unavoidable noises. As demonstrated by Romero and Dickey, the phase-only device either has a single nonzero Fourier component, or has an infinite number of nonzero Fourier components.\[52\] If we want to design a device with finite Fourier components with the phase-only method, such as a grating, this theorem means that the noises will always exist except for light deflection (a grating with only one diffraction order). Although researchers have exploited simultaneous control of amplitude and phase in recent years,\[30\] the efficiency is limited and it has not been generally applied in information photonics. In addition, most of the geometric phase–based multifunctional metasurfaces are conjugate for left-handed circularly polarized (LCP) and right-handed circularly polarized (RCP) incidences, leading to a shared information bits of the multifunctional metasurfaces. Here, we analyze the diffraction fields of the metasurfaces in \(k\)-space, and propose a theoretical design using full Fourier components to manipulate the optical fields, which could significantly boost the applications based on the proposed platform without noises in theory. The designed metasurface can convert the incident \(\sigma\) light to \(\tau\) light of different functionalities with predefined energy ratios, and the functionalities are not only limited to vortex beams.

The schematic of the designed spin-selective multifunctional metasurface is shown in Figure 1. For the traditional intensity-only designs, the diffractive devices suffer from high noises because the diffraction field is the superposition of two conjugated fields.\[66\] For example, an amplitude grating always has symmetric diffraction orders. Thus, researchers prefer phase-only designs to manipulate the diffraction fields, which also suffer from unavoidable noises due to the lack of full Fourier components.\[52\] In addition, the phase-only devices take optimization or iteration operations to maximize the efficiency, leading to time-consuming and complex designs. In contrast, our designs employ full Fourier components (intensity and phase) to manipulate the optical fields, which could significantly boost the applications based on the proposed platform without noises in theory. The designed metasurface can convert the incident \(\sigma\) light to \(\tau\) light of different functionalities with predefined energy ratios, and the functionalities are not only limited to vortex beams. Although independent control of amplitude and phase is a basic condition to realize energy tailorable multifunctional, we cannot design the metasurface by directly varying the amplitude of each channel because the energy of each channel is also associated with its phase distribution. For example, the deep sub-wavelength metasurface with identical phase delay in each unit cell can generate a plane wave front. However, the deep subwavelength metasurface with \(0\) and \(\pi\) phase delay in every other unit cell cannot scatter the incident wave to the far-field region since the phase gradient is much larger than the wave vector in free space, leading to evanescent waves near the metasurface. As an example, we calculated the diffraction field

**Figure 1.** Realization of the energy tailorable spin-selective multifunctional metasurface. a) Comparison between different methods to manipulate the optical fields in the diffraction zone. With full Fourier components manipulation, the diffraction field can be fully controlled with simple design, and with no noises in theory, while with intensity- or phase-only design, the applications are limited with intrinsic noises. Direct imaging means imaging directly using the transmission function without diffraction, such as a calibration test target. b) Schematic illustration of spin correlated three-channel vortex beams generated from the full-Fourier-component metasurface, in which the \(j\)th functionality \(|F_j>\) for \(\sigma\) incidence is designed with energy of \(\alpha_j\). The blocked channel for \(-\sigma\) incidence carries no information. c) The unit cell of the metasurface consists of an amorphous silicon elliptic nanopillar with height of 860 nm on the fused silica substrate. The short axis \(a\) and the orientation angle \(\theta\) (define as the crossing angle with \(y\)-axis) vary with the required transmission and phase, and the long axis \(b\) of the ellipse is set as 465 nm.
distribution for three different phase profiles, and the calculated total energy of the corresponding diffraction field varies from $1.33 \times 10^5$ to $2.48 \times 10^6$ for the designed three phase profiles (in arbitrary unit, see Figure S1 in the Supporting Information). To take phase distribution of each functionality of the metasurface into consideration, a momentum analysis method\(^{[33,53,54]}\) was adopted to calculate the far-field diffraction in \(k\)-space (defined as the functionality function)

\[
\mathcal{F}(k) = \sum_{j=1}^{M} |A_j| e^{-i(k \cdot r_j)} \prod_{x,y} \sin(k x, T_{MS}^{(j)}) k_x
\]

(1)

where \(t_i\), \(\phi_i\), \(r_i\), and \(T_{MS}^{(j)}\) indicate the electric transmission/reflectance, phase delay, spatial location, and equivalent size of each unit cell, respectively. For an arbitrary M-function metasurface, the total functionality function is the sum of each one

\[
\mathcal{F} = \sum_{j=1}^{M} \mathcal{F}_j
\]

(2)

The \(i\)th unit cell should be designed according to the formula \(A_i e^{-i\beta} = \sum_{j=1}^{M} |c_{ij}| A_j e^{-i\beta j}\), where \(A_j = \frac{t_j}{\pi} \prod_{x,y} \sin(k x, T_{MS}^{(j)}) k_x\) is the effective amplitude of the \(j\)th functionality and the \(i\)th unit cell, \(c_{ij}\) is a constant associated with the energy ratio of the \(j\)th functionality. To ensure that the effective amplitude is no more than one, we need to normalize and replace \(A_i\) with \(A'_i = \frac{A_i}{\max(A_i)}\). The total energy of the diffraction field is

\[
E = \int_{-k}^{k} |\mathcal{F}(k)|^2 dk
\]

Thus, the total energy can be written as

\[
E = \sum_{j=1}^{M} c_j E_j + \sqrt{\sum_{m} \sqrt{c_m e_n}} \int_{-k}^{k} \mathcal{F}_m(k) \mathcal{F}_n^*(k) dk
\]

(3)

where \(E_j = \int_{-k}^{k} |\mathcal{F}_j(k)|^2 dk\) is the total energy of the \(j\)th functionality. For simplicity, we assume the functionality channels do not interact with each other in \(k\)-space, which can be mathematically expressed with \(\mathcal{F}_j(k)|_{mk} = 0\). Thus, Equation (3) can be simplified according to \(\int_{-k}^{k} \mathcal{F}_m(k) \mathcal{F}_n^*(k) dk = \int_{-k}^{k} \mathcal{F}_n(k) \mathcal{F}_m^*(k) dk = \int_{-k}^{k} \mathcal{F}_m(k) \mathcal{F}_n^*(k) dk = 0\), where \(m \neq n\). The total energy of \(\mathcal{F}\) is

\[
E = \sum_{j=1}^{M} c_j E_j
\]

(4)

Thus, by employing full Fourier components \(A'_j\) and \(\phi_j\), the control of energy ratio of \(\mathcal{F}\) could be realized. The energy ratio is defined as \(\alpha_j = c_j E_j / E\). Since the full Fourier components could completely describe the diffraction fields of the devices, we do not need to further optimize to maximize the efficiency.

The proposed metasurfaces are designed with amorphous silicon nanopillars for the operation wavelength of 1550 nm. Such large aspect-ratio dielectric structures with high refraction index can generate waveguide modes\(^{[54,55]}\) and support Fabry–Pérot resonances,\(^{[56,57]}\) leading to deep modulation of optical amplitude,\(^{[58]}\) phase,\(^{[59,60]}\) and polarization.\(^{[61]}\) We optimized the silicon nanopillars with height of 860 nm for different diameters and orientations to realize the required optical modulation (Figure 1c). The simulated nanopillar with short axis of 270 nm and long axis of 465 nm serves as an efficient half-wave plate with transmission of 0.97, which can convert the incident polarization to its orthogonal state (see Figure S2 in the Supporting Information). The fabricated metasurface is shown in Figure 2a. With the increasing of the short axis, the transmission of the cross-polarized light gradually decreases to zero until the length of short axis equals to that of the long axis (Figure 2b). This is because the nanopillar becomes symmetric in \(x-y\) plane when the ellipse turns to be a circle, unable to realize polarization conversion anymore. The nanopillars possess propagation phase and geometric phase simultaneously.\(^{[33,62]}\) For LCP/RCP incidence, the simulated propagation phase delay of the nanopillars varies over 1.25\(\pi\) for different lengths of short axis (with the orientation angle \(\theta = 0\)). In Figure 2c,d we depicted the geometries and orientations of the nanopillars for any predefined phase and transmission with LCP/RCP incidence. The phase can be written as \(\phi = \Phi_0 + 2\pi\sigma\theta\), where \(\Phi_0\) is the propagation phase and \(\sigma = \pm 1\) is the helicity of the incident light. For a given \(\phi\), the orientation angle is \(\theta = (\phi - \Phi_0)/2\pi\), which varies with \(\Phi_0\) and \(\sigma\). As a result, although the propagation phase for LCP/RCP incidence is the same and shows no chirality, the orientation angles of the nanopillars differ from each other for LCP/RCP incidence, which induces spin-selective functionalities and chirality of the metasurfaces. This intriguing property introduced by group effects of the nanopillar arrays will be discussed in detail in the following parts. The waveguide modes in large aspect-ratio dielectric nanopillars usually lead to broadband responses. We simulated the transmission and phase delay of the nanopillars for different lengths of short axis over 1200 to 1800 nm, where the orientation angle \(\theta\) is fixed as 0 (Figure 3a,b). The simulated results show a broadband high-transmission area accompanied with three resonant lines cutting the spectra. The linewidths of such resonances are generally very narrow due to the rigid condition to realize Fano resonances.\(^{[63-66]}\) The high-transmission areas dominate most of the transmission spectra. The simulated phase is more smooth and covers [0, 2\(\pi\)] for the selected waveband. Four resonant waveguide modes marked in Figure 3a are also shown in Figure 3c, which shows near field magnetic distributions of the nanopillars. The light energy is mainly confined inside the nanopillar and has negligible dependence on the neighboring nanopillars, which is a basic condition to locally control the scattered EM field.\(^{[51,54]}\) With the decreasing of the wavelength, the number of wave loops will increase due to the decreasing of effective wavelength \(\lambda_{\text{eff}}\), where \(n_{\text{eff}}\) is the effective refractive index of the dielectric waveguide and can be computed through a step-index circular waveguide model. Such results show that although the designed metasurfaces are not broadband, the proposed design could be easily changed to other waveband by adjusting the length of the axis.

We employed the proposed theory and simulated nanopillars to realize the energy tailorable multifunctional metasurfaces. The electron-beam lithography was adopted to fabricate the metasurfaces with squared subwavelength lattice. The radii of the fabricated metasurfaces are 50 \(\mu\)m. A custom-built setup is used to measure different functionality channels in \(k\)-space.
As an example, we designed four samples with three channels in each one. The three channels were a three-order vortex beam ($F_1$), a one-order vortex beam ($F_2$), and a plane wave ($F_3$), respectively. The transmitted RCP waves were detected for LCP incidence. We obtained the numerical intensity matrix of the light field in $k$-space using the LABVIEW-based InGaAs camera, and integrated the matrix within each functionality area to quantify its energy. We also theoretically calculated the energy following the formula $E_k = \int |\mathcal{F}(k)|^2 dk$.

As shown in Figure 4b, the calculated and measured energy ratios are close to the designed ones, demonstrating the validity of the proposed theory. The theoretically calculated energy distributions for the four samples are shown in Figure 4c–f. Compared with the theoretical calculation, the measured energy distributions also show the evident energy variation in each channel but with zero-order light in the center, which is also the original point of $k$-space (Figure 4g–j). The zero-order light is attributed to imperfections of fabrication and measurement, and could be easily blocked by a Fourier filter in real applications. It is worth mentioning that the larger the metasurface is, the sharper the functionality channel in $k$-space will be.\cite{67,68}

We also simulated the field distribution for a designed metasurface with radius of 16 $\mu$m (see Figure S4 in the Supporting Information). We extracted the field distribution at a cut plane with 5 $\mu$m from top of the nanopillars, and performed fast Fourier transform (FFT) with MATLAB to get the simulated field in $k$-space, which is in good agreement with the theory and experiments. The theoretical efficiency of the design is about 40%, which is lower than phase-only multifunctional metasurfaces. The proposed design provides an alternative method to those applications in which low noises is more pivotal.
Figure 3. The resonance behavior of the nanopillars to realize the energy tailorable spin-selective metasurfaces. a, b) Simulated transmission (a) and phase delay (b) (normalized with \( \pi \)) at a broad wavelength range with different lengths of short axis of the nanopillars. The black dashed lines indicate sharp Fano resonances, which lead to an abrupt change in the transmission spectra. c) Magnetic intensity distribution at four positions marked in (a) with \( a = 292 \) nm, which shows different waveguide modes of the nanopillars.

As discussed above, the designed metasurfaces possess spin-selective and chiral behaviors considering their group functionalities. Although the cross-polarized transmission and propagation phase remain the same for LCP and RCP incidences, the nanopillars play different roles in the metasurfaces for different incident polarizations. For example, for LCP incidence, we randomly selected three nanopillars with \( |t_{RL1}| = 0.97, \phi_{RL1} = \pi; |t_{LR2}| = 0.62, \phi_{LR2} = \pi/2; |t_{RL3}| = 0.15, \phi_{RL3} = 0 \), the corresponding transmission and phase delay for RCP incidence will be \( |t_{RL1}| = 0.97, \phi_{RL1} = -0.52\pi; |t_{LR2}| = 0.62, \phi_{LR2} = -1.24\pi; |t_{RL3}| = 0.15, \phi_{RL3} = -1.52\pi \), whose phase distributions are random compared with those of the LCP incidence. That means if we design the phase distribution of the multifunctional metasurface with predefined LCP incidence, the metasurface will lose the information of the wave front for RCP incidence, and vice versa. As shown in Figure 5a, we measured the energy distribution for RCP incidence at the focal plane, and the energy is low and dispersive (blocked channel), demonstrating the spin-selective behavior of the designed metasurfaces. It is worth noting that this spin-selective characteristic originates from the arrangements of massive unit cells, and is one of the group functionalities. Although the transmission of the nanostructures shows no chirality, the spin-selective behavior is related to the transmission phase and Pancharatnam–Berry phase, simultaneously. Another application is to achieve the calibration test target. As shown in Figure 5b, we employed high polarization conversion pixels \( (a = 270 \text{ nm}, b = 465 \text{ nm}) \) and no-polarization conversion pixels (cylindrical pixels) to realize high-contrast 1951 USAF resolution test target, with orders of 6 and 7. For LCP-RCP or RCP-LCP conversion, the designed target is a negative one, and for LCP-LCP or RCP-RCP conversion, it is a positive one. Interestingly, compared with the blocked channels in the vortex beams generation, the calibration metasurfaces maintain the same number of channels for different polarization conversion. This is due to the symmetry of the rotation-free dielectric pixels. The calibration design also demonstrates that the proposed platform can combine the intensity- and phase-only applications together.

Our theory is not only limited to vortex beams. Any designs with weak interference between different channels in \( k \)-space are also suitable. We designed a two-function metasurface, which can combine metasheets and anomalous refraction simultaneously. The schematic of the design is shown in Figure 6a. The designed metasheets occupies a phase distribution of \( \phi_i = -k_i \left( \sqrt{r^2 + f^2} - f \right) \) with focal length of \( f = 40 \text{ \mu m} \), and the anomalous refraction has a phase distribution of \( \phi_2 = -0.2k_0x \) with refraction angle of \( 11.5^\circ \). The total size of the metasurface is 200 \( \mu \text{m} \). We combined the two functionalities with different energy ratios following the proposed theory, and compared the calculated and designed energy ratios in Figure 6b. It turns out that the two results meet well with each other, demonstrating that the proposed theory can be applied to realize versatile functionalities, with high accuracy and broad design range (from \( 2^{-4} \) to \( 2^4 \)). We also calculated the intensity distribution in \( k \)-space for \( \alpha_2/\alpha_1 = 1 \) (Figure 6c). For the metasheets, most of the energy distributes at large \( k \) components. For
the anomalous refraction, the energy locates at $-0.2k_0$, showing a $\delta$-function-like profile. On the other hand, for the metalens, most of the energy is confined at the focal point. The intensity of the electric field of the metalens is much smaller than that of the anomalous refraction at areas away from the focal point. Thus, the functionalities of the metasurface can also be distinguished in real space (Figure 6c, d).

If existing weak interference in $k$-space between different channels, the energy tailorable functionality can also be realized to meet the scalar superposition condition in Equation (4). However, this limitation can be further released if we can find a method or a space to separate the overlapping functionalities. The interference factor in Equation (3) can be eliminated via transformation of coordinates in $k$-space, which also means de-multiplexing in a new space/coordinate. One of the possible methods to realize this strategy may be utilizing multilayer metasurfaces, which have recently been adopted to correct chromatic aberrations of metalenses. The spin-selective behavior, which is attributed to a group effect, occurs when numerous nanopillars gather in one device. It is known that group effects are mainly associated with symmetries, such as topological photonics and phononics. Such intriguing properties may have deep impact on theoretical design of planar integrated devices.

In summary, the energy tailorable spin-selective metasurfaces, which can precisely control the energy configuration with a spin-selective behavior, are demonstrated. We utilized the momentum analysis method to deal with the field distribution of each functionality, and in return to compute the energy configuration of the integrated metasurfaces. The design strategy has been demonstrated by the amorphous silicon nanopillars, which can efficiently manipulate the full Fourier components of optical fields. The measured, calculated, and predefined energy distributions can match with each other in a broad design range. The spin-selective behavior of the multifunctional metasurfaces is resulting from a group effect with numerous nanopillar arrays, although a single nanopillar shows no chirality. The spin-selective calibration test targets were also demonstrated. The proposed design strategy is suitable for any integrated functionalities with weak interference in $k$-space between different

![Figure 4](imageURL)

**Figure 4.** Demonstration of the energy tailorable multifunction with LCP incidence. a) The incident polarization is controlled by a polarizer (LP1) and a quarter-wave plate (CP1). The output light is collected by an objective (Obj) and a tube lens (TL), and the transmitted polarization is detected by a quarter-wave plate (CP2) and a polarizer (LP2). Then, a Fourier lens (FL) and an InGaAs camera are adopted to measure the far-field diffraction in $k$-space. b) The designed, calculated and measured energies of each functionality of the four metasurface samples, in which $|F_1|$, $|F_2|$, $|F_3|$ are designed as vortex light with order of 3, 1, 0, respectively. Theoretical $|E|^2$ distributions of three functionalities in $k$-space for different designed samples. c–f) Theoretical $|E|^2$ distributions of three functionalities in $k$-space for different designed samples. g–j) Measured light distributions of three functionalities in $k$-space, which are obtained from measured numerical intensity matrices. The insets in (g–j) show the enlarged images of each functionality in 2 mm defocusing plane captured with an InGaAs camera.
were simulated through finite element method (FEM)-based COMSOL wet etching method before optical measurement. Cr resist was remove by wet etching method. Finally, a 3 nm Cr layer was evaporated deposition (EBD) method. Then the Cr film was striped by pure water for 60 s and PMMA was developed with MIKE\IPA(1:3) for 40 s. After the EBL process, the Pedot:PSS layer was removed with hot acetone at degree of 60 °C. Then a 35 nm were spin coated on the substrate by sequence. The dielectric metasurfaces were fabricated on a fused silica substrate. First, a layer of 860 nm amorphous silicon was coated on the substrate with plasma enhanced chemical vapor deposition (PECVD) method at the temperature of 380 °C. Then a layer of PMMA with thickness of 200 nm and a layer of Pedot:PSS with thickness of 35 nm were spin coated on the substrate by sequence. The field distribution was extracted at a cut plane with 5 µm from top of the nanopillars, and the field distribution was simulated for a designed metasurface with radius of 16 µm (see Figure S4 in the Supporting Information). The field distribution was simulated through finite element method (FEM)-based COMSOL Multiphysics to find the resonances of the structure. With σ incidence (σ = ± 1 indicates LCP/RCP light), the amplitude and phase of the transmitted −σ components were computed by the electric projection ⟨−σ E⟩. The permittivity of the amorphous silicon was taken from ref. [70], and the substrate was fused silica with refractive index of 1.5. During the simulation, the incident light was set at the substrate side to guarantee that the transmitted light propagates in free space. After finding a nanopillar serving as a perfect half-wave plate at 1550 nm, the short axis of the ellipse was gradually increased to get a decreasing amplitude modulation. The phase modulation was realized through Pancharatnam–Berry phase and propagation phase. The group effects of the multifunctional metasurfaces were calculated through the momentum analysis method,[53] which can conveniently handle the field distributions in k-space. The energy distribution was integrated for each functionality channel of the calculated field in k-space, and the calculated energy intensity was obtained in Figure 4b. Also, the field distribution was simulated for a designed metasurface with radius of 16 µm (see Figure S4 in the Supporting Information). The field distribution was extracted at a cut plane with 5 µm from top of the nanopillars, and fast Fourier transform (FFT) was performed with MATLAB to get the simulated field in k-space.

Measurement Procedure: The measurement setup consisted of a super-continuous laser (NKT SuperK EXR-20, λ = 1550 nm) whose polarization was controlled by a linear polarizer and a quarter-wave plate pair to get LCP/RCP incidence. Another quarter-wave plate and linear analyzer pair were utilized to acquire the RCP/LCP output components of the sample. Since only the cross-polarization light was detected, the co-polarization light would not be the noise background of the signal even the size of the incident light beam is much larger than that of the sample. The transmitted signal was collected by an objective (Sigma Near Plan Apo 50×, NA = 0.67) and a tube lens (Thorlabs, TL200-3P). Then, a Fourier lens was adopted to realize Fourier transform of the transmitted signal at its focal plane, which was imaged by an InGaAs camera (HAMAMATSU InGaAs C10833). The measured energy channels. Our approach does not suffer from intrinsic noises and complex optimization processes, and can find some applications in optical concurrent communication, computation, and imaging diagnostics.

Experimental Section

Sample Fabrication: The dielectric metasurfaces were fabricated on a fused silica substrate. First, a layer of 860 nm amorphous silicon was coated on the substrate with plasma enhanced chemical vapor deposition (PECVD) method at the temperature of 380 °C. Then a layer of PMMA with thickness of 200 nm and a layer of Pedot:PSS with thickness of 35 nm were spin coated on the substrate by sequence. The Pedot:PSS layer was intended for charge release during the electron-beam lithography (EBL) process employing a 100 kV voltage, 200 pA current, and 950 µC cm−2 dose. To control the lateral size of nanopillars, Beamr, a software from Genysis ltd., was employed to rescale the layout pattern considering the process broadening. As a result, the scale precision of the nanopillars with random angles can be as high as less than 10 nm. After the EBL process, the Pedot:PSS layer was removed with pure water for 60 s and PMMA was developed with MIKE\IPA(1:3) for 40 s. Then a 50 nm Cr layer was deposited on the resist with electron beam evaporation deposition (EBD) method. Then the Cr film was striped by removing PMMA with hot acetone at degree of 60 °C for 20 min, which was followed by HBr plasma dry etching with ICP machine. The residue Cr resist was remove by wet etching method. Finally, a 3 nm Cr layer was coated for scanning electron microscopy (SEM) and then removed with wet etching method before optical measurement.

Simulation and Design: The amorphous silicon elliptic nanopillars were simulated through finite element method (FEM)-based COMSOL Multiphysics to find the resonances of the structure. With σ incidence (σ = ± 1 indicates LCP/RCP light), the amplitude and phase of the transmitted −σ components were computed by the electric projection ⟨−σ E⟩. The permittivity of the amorphous silicon was taken from ref. [70], and the substrate was fused silica with refractive index of 1.5. During the simulation, the incident light was set at the substrate side to guarantee that the transmitted light propagates in free space. After finding a nanopillar serving as a perfect half-wave plate at 1550 nm, the short axis of the ellipse was gradually increased to get a decreasing amplitude modulation. The phase modulation was realized through Pancharatnam–Berry phase and propagation phase. The group effects of the multifunctional metasurfaces were calculated through the momentum analysis method,[53] which can conveniently handle the field distributions in k-space. The energy distribution was integrated for each functionality channel of the calculated field in k-space, and the calculated energy intensity was obtained in Figure 4b. Also, the field distribution was simulated for a designed metasurface with radius of 16 µm (see Figure S4 in the Supporting Information). The field distribution was extracted at a cut plane with 5 µm from top of the nanopillars, and fast Fourier transform (FFT) was performed with MATLAB to get the simulated field in k-space.

Figure 5. Measured spin-selective behaviors of the metasurfaces. a) Measured LCP light distributions for RCP incidence in the focal plane of Sample #1. b) Measured light distributions for direct imaging of 1951 USAF resolution test target designed with the metasurface (Sample #5). For LCP incidence, the transmitted image of RCP/LCP light is a negative/positive target, respectively. For RCP incidence, similar phenomena can also be observed. c) The number of information channels the light beam carries. For LCP-RCP conversion, the light carries three channels (Sample #1–#4), while for RCP-LCP conversion the information channel is blocked (Sample #1–#4). As a contrast, for Sample #5 the light carries the same information channels for LCP-RCP and RCP-LCP conversion. Note that we do not define the exact value of the number of channels for Sample #5, since the resolution test target is an image.
Energy tailorable anomalous refraction and focusing. a) Schematic of the multifunctional metasurface that can simultaneously realize anomalous refraction ($|F_1>\rangle$) and focusing ($|F_2>\rangle$), with arbitrarily designed energy assignment. b) Calculated energy ratio of $\alpha_2/\alpha_1$ (red dotted line) as a function of the designed energy ratio. The gray dashed line indicates that the calculated energy ratios equal to the designed ones. c) Calculated logarithmic intensity distribution near the focal point. d) The electric field distribution of the anomalous refraction away from the focusing area. e) The $|E|^2$ distribution near the focal point.

was acquired through the following method. First, the intensity matrix without incident light $\eta$ was obtained by a LABVIEW-based InGaAs camera. Second, the intensity matrix at the focal plane of the Fourier lens $x$ was captured using the same method. Third, the final intensity matrix calculated with $x-\eta$ was imported to a data analysis software MATLAB to integrate the total energy in each functionality area. Then, we used zero-order light as the origin of the coordinate, and used the distance between zero-order light and $F_1$ to calibrate the dimensions in $k$-space.

**Conflict of Interest**

The authors declare no conflict of interest.

**Keywords**

Fourier optics, information optics, metasurfaces, multifunction, spin

Selectivity

**Supporting Information**

Supporting Information is available from the Wiley Online Library or from the author.

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